

Convective meta-thermal concentration for Stirling engine

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I. Introduction

The Stirling engine possesses several advantages, including external combustion characteristics, a simple structure, and high theoretical thermal efficiency. Extensive research has been conducted on its potential for waste heat and cold utilization, which can greatly enhance energy efficiency [1]. However, the engine suffers from thermal inefficiency due to the temperature variations in practical heat-exchanging fluids [2-4]. To address this issue, convective meta-thermal concentration (CMTC) was introduced in this study as a means of improving the Stirling engine system. By increasing the temperature difference between the hot and cold ends, a significant improvement in the engine's efficiency was achieved.

II. Theoretical analysis

Fig. 1(a) shows a Stirling engine system integrated with CMTC. A more detailed relationship between input [output] heat flux \dot{Q}_{HE}^u [\dot{Q}_{CE}^u] and the temperature of the working substance on the hot [cold] end T_{HE}^u [T_{CE}^u] is presented in Fig. 1(b). Note that, $u = Cl$ and $u = TCP$ represents the shells of the heat and cooler are made by classical high thermal conductivity materials (Cl shell) and high-low thermal conductivity materials alternatively arranged [Thermal conductivity platter (TCP) shell], respectively. Compared with the Cl shell, the TCP shell uses equivalent anisotropic thermal conductivity to concentrate heat flow, thereby acting as CMTC. By implementing CMTC, the hot/cold end temperature can be increased/decreased [Fig. 1(c)]. Coupling this effect into the Stirling engine system, the engine power could be improved [Fig. 1(d)]. Assuming the Stirling engine undergoes an internal reversible cycle, its thermal efficiency reads

$$\eta_u = 1 - \frac{T_{CE}^u(\dot{Q}_{CE}^u)}{T_{HE}^u(\dot{Q}_{HE}^u)}$$

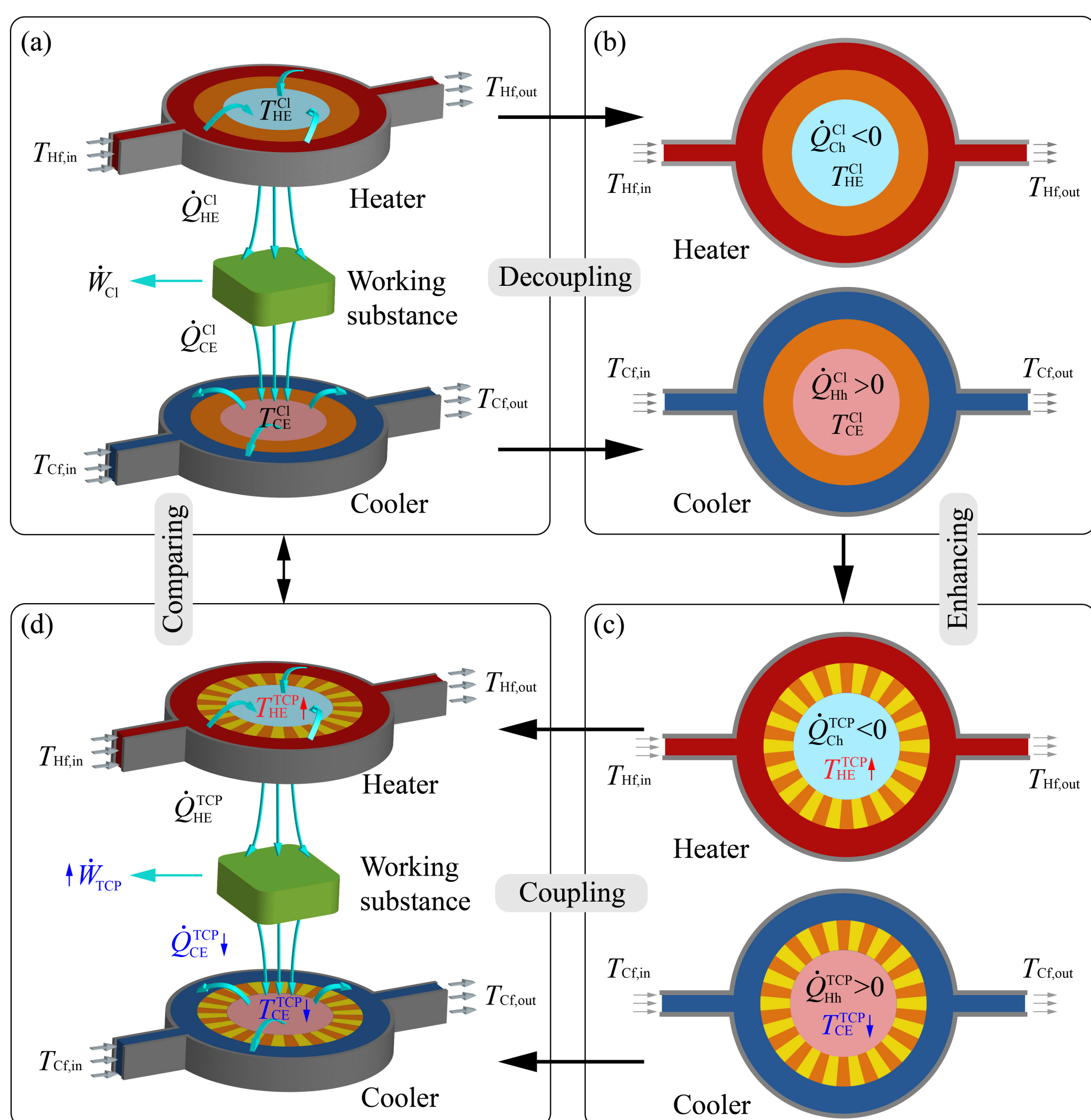


Fig. 1. Schematic diagram of the Stirling engine system with and without CMTC [5].

Define heating and cooling enhancement coefficients as $\alpha = T_{HE}^{TCP} / T_{HE}^{Cl}$ and $\beta = T_{CE}^{TCP} / T_{CE}^{Cl}$, respectively. The thermal efficiency improvement magnitude from the Stirling engine without CMTC to that with CMTC can be expressed as

$$\zeta = \frac{\eta_{TCP} - \eta_{Cl}}{\eta_{Cl}} = \left(\frac{1}{\eta_{Cl}} - 1 \right) \left(1 - \frac{\beta}{\alpha} \right).$$

When \dot{Q}_{HE}^u is large enough, the Stirling engine efficiency without CMTC (η_{Cl}) will tend to 0 quickly due to the fast closing of T_{HE}^{Cl} and T_{CE}^{Cl} . At this time, if CMTC plays a significant role, making $\alpha \gg 1$ and $\beta \ll 1$, ζ will tend to ∞ . Then, an ultrahigh thermal efficiency improvement can be realized.

III. Results and discussion

We calculated the Stirling engine efficiency with and without CMTC under specific operating conditions, as shown in Fig. 2. When $\eta_{Cl} \rightarrow 0$, $\zeta \rightarrow 900\%$, which is in great consistent with the theoretical prediction.

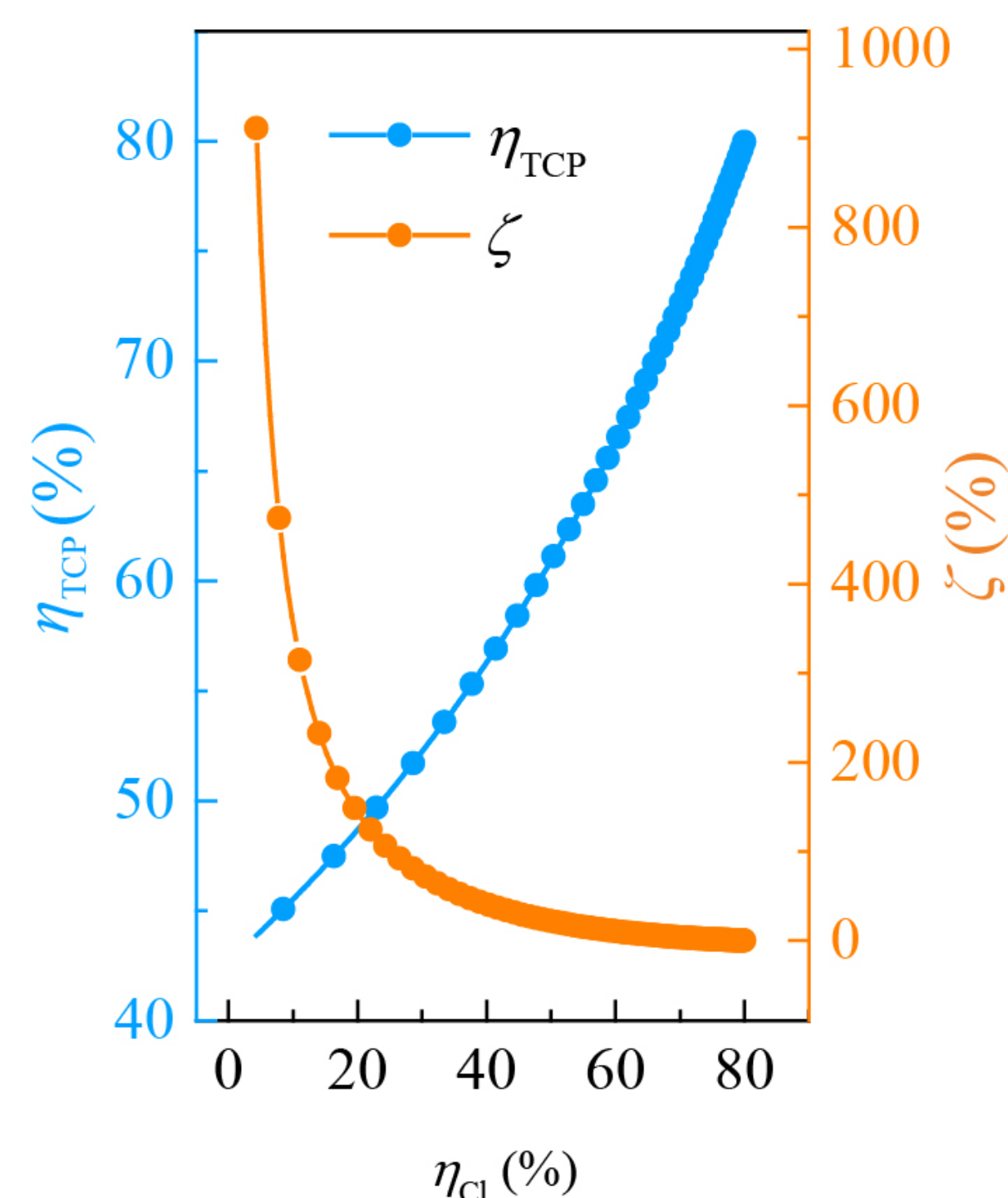


Fig. 2. Effect of CMTC on Stirling engine efficiency improvement [5].

It shows that when the Stirling engine efficiency is constrained by finite waste heat and cold resources, the integration of CMTC plays a crucial role in overcoming these limitations. This operation offers an exciting avenue for sustainable energy utilization.

IV. Conclusions

- CMTC significantly increases the temperature difference between both ends of the Stirling engine.
- When η_{Cl} is low due to the finite waste heat and cold resources, CMTC exhibits great potential for enhancing the Stirling engine efficiency.
- More operation conditions should be performed to further reveal the effect of CMTC for practical applications.

References:

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