

Mode-expansion theory for inhomogeneous meta-surfaces

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(submitted to PRB)

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I. Motivations:

In previous works of gradient meta-surface, theoretical understandings were either based on heuristic Fermat-Huygens wave interference arguments or based on full-wave numerical simulations^{1,2,3}.

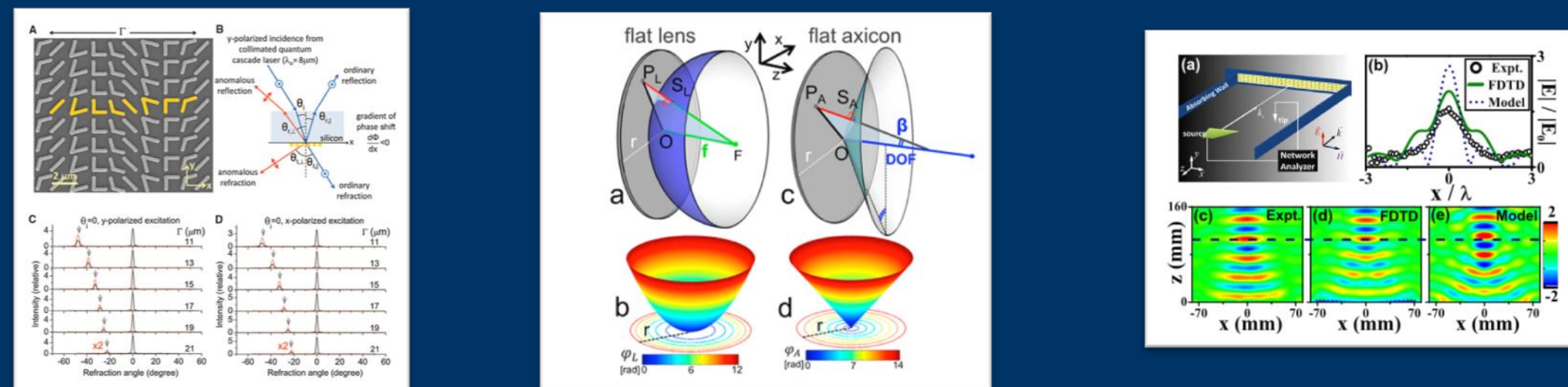


Fig. 1 Gradient meta-surface

PROBLEMS !

Is
Fermat-Huygens
enough?

Lack a theory
framework

Parabolic reflection-phase distribution:

$$\Phi(x) = \Phi_0 - k_0 \sqrt{x^2 + l_{focus}^2} + k_0 \cdot l_{focus}$$

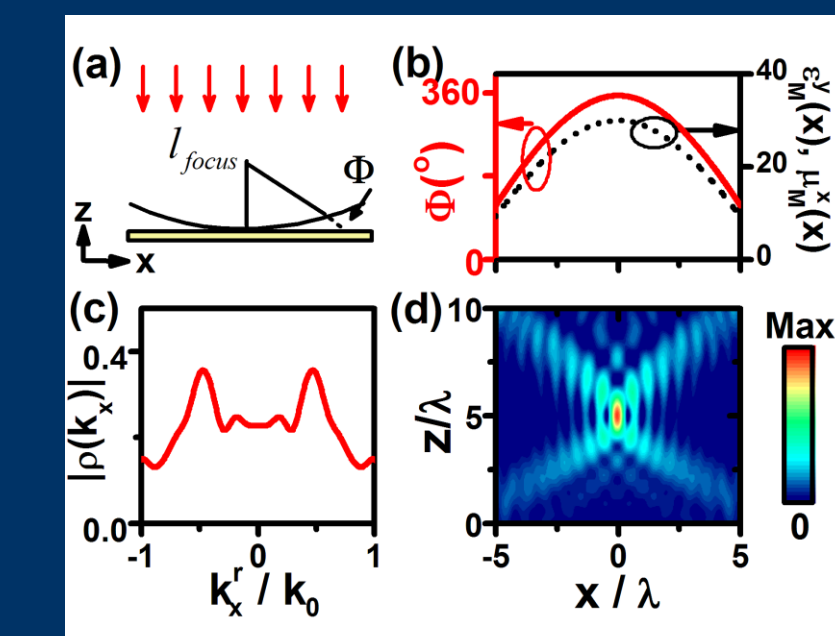


Fig.5 (a) Working scheme of the flat meta-surface lens, (b) Distributions of the parameter values and the reflection-phase. (c) Calculated spectrum. (d) Calculated E-field distribution .

II. Developments of the mode-expansion theory

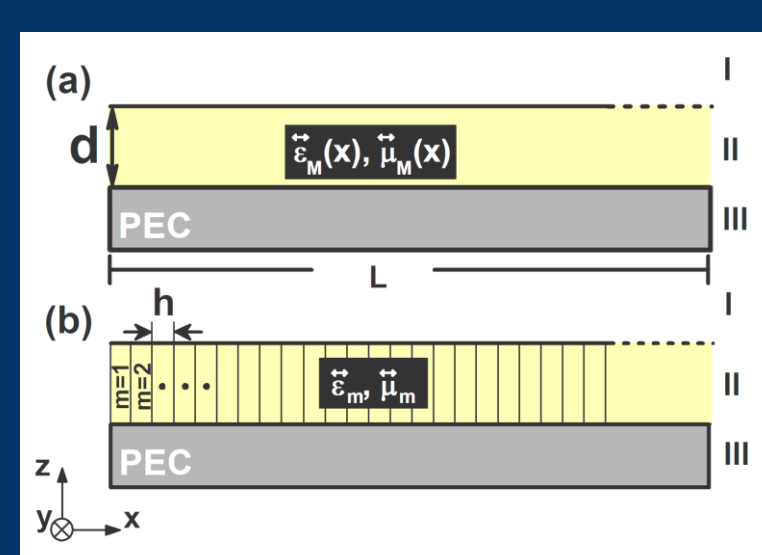


FIG. 2 (a) Geometry of the system under study. (b) Discretized model for the inhomogeneous structure.

The inhomogeneous MTM with permittivity and permeability matrices given by

$$\tilde{\epsilon}_M(x) = \begin{pmatrix} \epsilon_M^x(x) & 0 & 0 \\ 0 & \epsilon_M^y(x) & 0 \\ 0 & 0 & \epsilon_M^z(x) \end{pmatrix}, \tilde{\mu}_M(x) = \begin{pmatrix} \mu_M^x(x) & 0 & 0 \\ 0 & \mu_M^y(x) & 0 \\ 0 & 0 & \mu_M^z(x) \end{pmatrix}$$

Incident and reflected wave:

$$\begin{cases} \vec{E}^{\text{in}}(\vec{r}) = e^{i(k_x^{\text{in}}x - k_z^{\text{in}}z)} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \\ \vec{H}^{\text{in}}(\vec{r}) = -\frac{1}{Z_0} e^{i(k_x^{\text{in}}x - k_z^{\text{in}}z)} \begin{pmatrix} k_z^{\text{in}}/k_0 \\ 0 \\ k_x^{\text{in}}/k_0 \end{pmatrix} \end{cases} \quad \begin{cases} \vec{E}^{\text{ref},n}(\vec{r}) = e^{i(k_x^{\text{ref},n}x + k_z^{\text{ref},n}z)} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \\ \vec{H}^{\text{ref},n}(\vec{r}) = \frac{1}{Z_0} e^{i(k_x^{\text{ref},n}x + k_z^{\text{ref},n}z)} \begin{pmatrix} k_z^{\text{ref},n}/k_0 \\ 0 \\ -k_x^{\text{ref},n}/k_0 \end{pmatrix} \end{cases}$$

Here, $k_0 = \omega/c$ is the wave vector in vacuum with ω being the working frequency and c the speed of light.

The eigenmode in meta-surface region is:

$$E_y^{\pm}(q_z, x, z) = G(q_z, x) e^{\mp i q_z z}$$

where superscript, + and - stands for forward (+) and backward (-) propagating waves.

Here, G-function should be the result of

$$\frac{\mu_M^x(x)}{\mu_M^z(x)} \frac{d^2 G(q_z, x)}{dx^2} + [k_0^2 \epsilon_M^y(x) \mu_M^x(x) - q_z^2] G(q_z, x) = 0$$

Matching boundary condition

$$\begin{cases} e^{ik_x^{\text{in}}x} + \sum_n \rho(k_x^{\text{ref},n}) e^{ik_x^{\text{ref},n}x} = \sum_j G(q_{z,j}, m) [C^+(q_{z,j}) + C^-(q_{z,j})] \\ \frac{k_x^{\text{in}}}{k_0} e^{ik_x^{\text{in}}x} - \sum_n \rho(k_x^{\text{ref},n}) \frac{k_x^{\text{ref},n}}{k_0} e^{ik_x^{\text{ref},n}x} = \sum_j \frac{q_{z,j}}{\mu_M^x k_0} G(q_{z,j}, m) [C^+(q_{z,j}) - C^-(q_{z,j})] \end{cases}$$

Reflection coefficients:

$$\rho(k_x^{\text{ref},n}) = \sum_j A^{-1}(k_x^{\text{in}}, q_{z,j}) B(q_{z,j}, k_x^{\text{ref},n})$$

where we have introduced two matrixes defined as:

$$\begin{cases} A(q_{z,j}, k_x^{\text{in}}) = \frac{k_z^{\text{ref},n}}{k_z^{\text{ref},n} + k_z^{\text{in}}} S(q_{z,j}, k_x^{\text{ref},n}) + \frac{k_z^{\text{in}}}{k_z^{\text{ref},n} + k_z^{\text{in}}} S'(q_{z,j}, k_x^{\text{ref},n}) \\ B(q_{z,j}, k_x^{\text{ref},n}) = \frac{k_z^{\text{in}}}{k_z^{\text{ref},n} + k_z^{\text{in}}} S(q_{z,j}, k_x^{\text{ref},n}) - \frac{k_z^{\text{ref},n}}{k_z^{\text{ref},n} + k_z^{\text{in}}} S'(q_{z,j}, k_x^{\text{ref},n}) \end{cases}$$

with

$$\begin{cases} S(q_{z,j}, k_x^{\text{ref},n}) = \frac{1}{L} \sum_m h(1 - e^{-i2q_{z,j}d}) G(q_{z,j}, m) e^{-ik_x^{\text{ref},n}mh} \\ S'(q_{z,j}, k_x^{\text{ref},n}) = -\frac{1}{L} \sum_m h \frac{q_{z,j}}{\mu_M^x k_0} (1 + e^{-i2q_{z,j}d}) G(q_{z,j}, m) e^{-ik_x^{\text{ref},n}mh} \end{cases}$$

III. Applications of the theory

Linearly varying reflection-phase profile:

$$\Phi(x) = \Phi_0 + \xi x$$

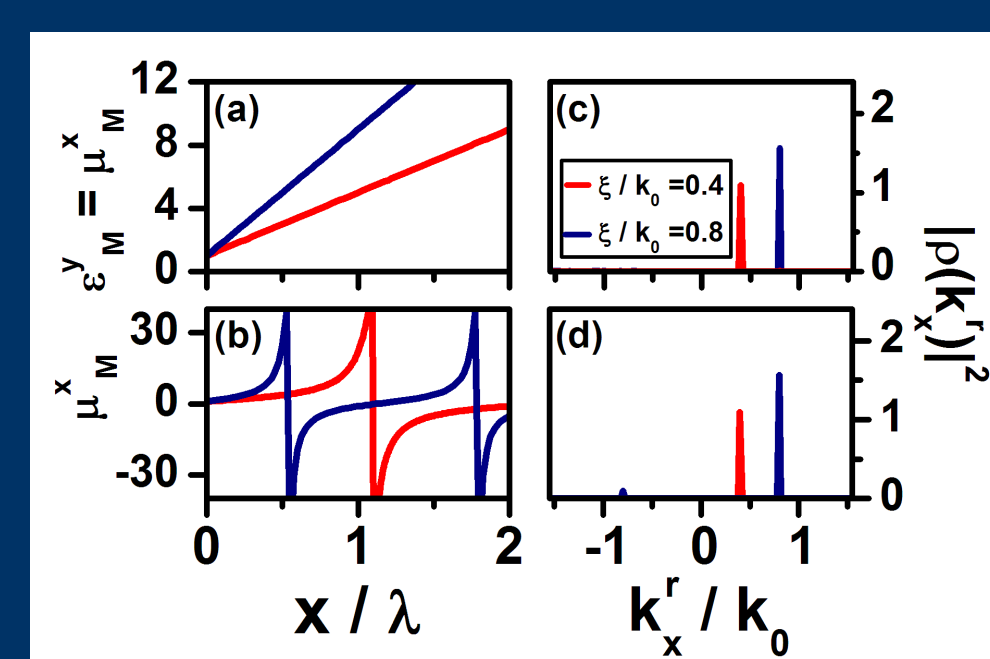


Fig.3 (a) Material properties. (b) Calculated scattering coefficients. (c) Calculated scattering coefficients. (d) Calculated scattering coefficients.

The generalized Snell's law:

$$k_x^{\text{ref}} = \xi + k_x^{\text{in}}$$

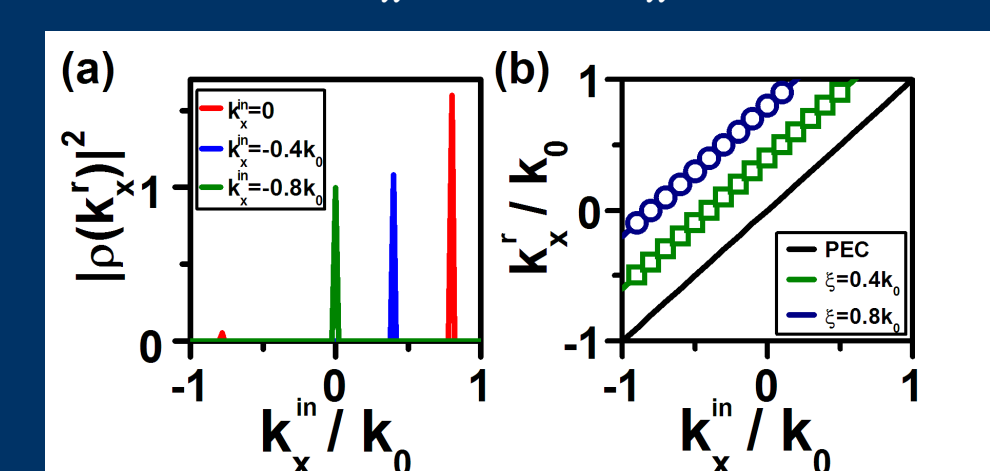


Fig.4 (a) Calculated scattering coefficients (b) angler dependency.

IV. Comparisons with the local response model

With local approximation and neglecting near-field correction.

$$\rho_{\text{LRM}}(k_x^{\text{ref}}) = -e^{2ik_0d} \delta(k_x^{\text{ref}} - k_x^{\text{in}} - \xi)$$

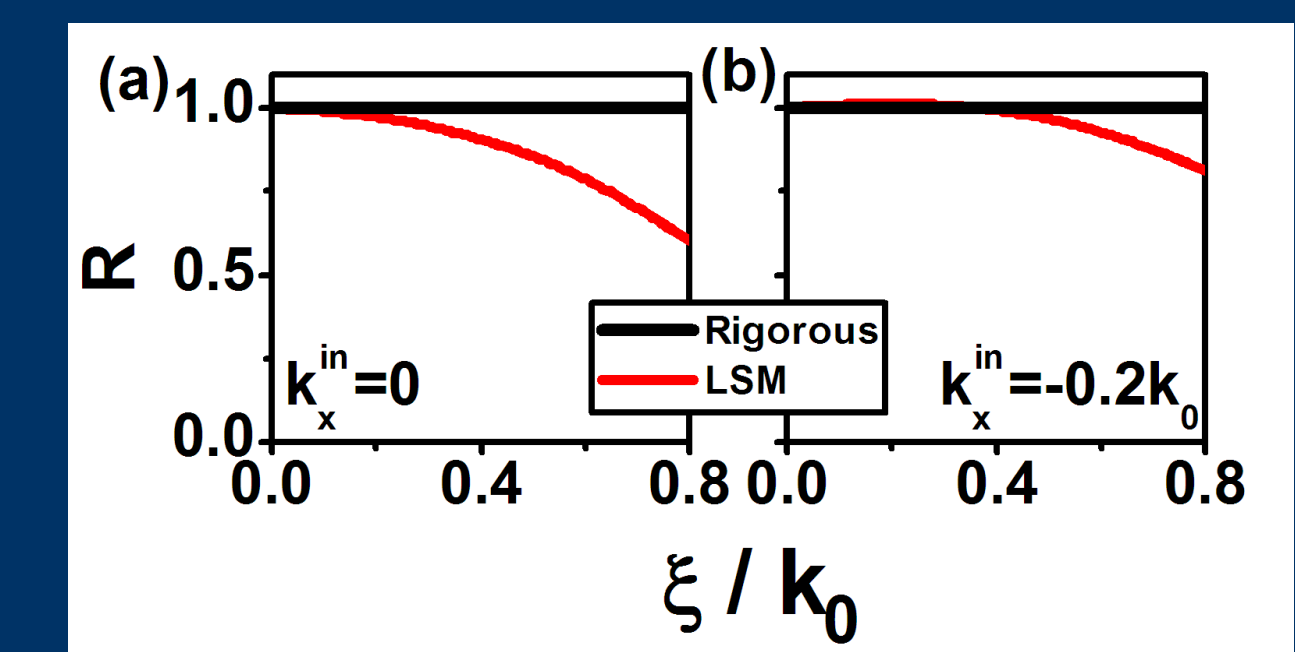


FIG. 6. (color online) Calculated reflectance of rigorous mode expansion method (black line) and local model (red line) versus ξ/k_0

V. Experimental and simulation verifications

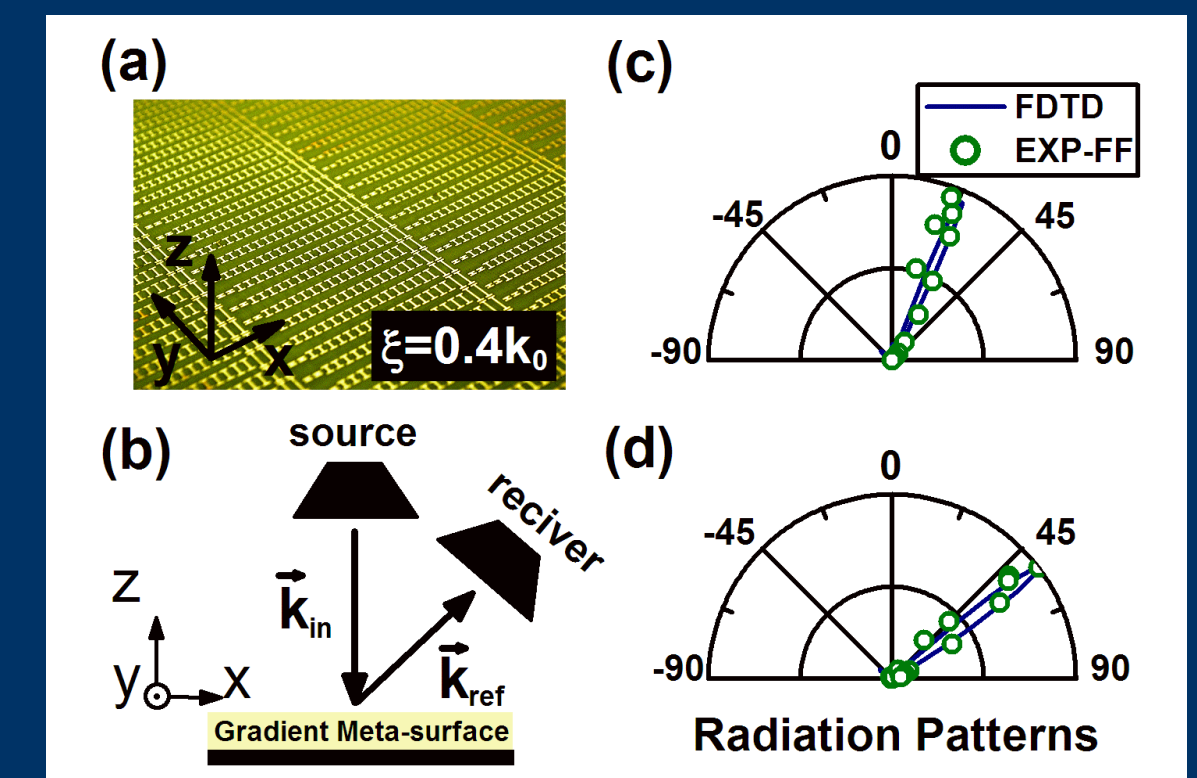


Fig.7. (a) Picture of part of the fabricated sample. (b) Schematics of the far-field characterization. (c) and (d) Measured (scatters) and simulated (lines) scattering patterns.

Conclusions:

- 1) Established a general theoretical framework.
- 2) Applied it to two particular examples as applications.
- 3) Full theory could go back to local response model under several simplifications.
- 4) local response model has energy non-conservation problems.
- 5) Microwave experiments match theoretical predictions .